

M.Tech (Structural Engg.)

MSEPC 1030 - Matrix Method of Analysis
of Structure

Answer key.

PART. A.

a. Degree of redundancy = 1

b. Kinematic indeterminacy = 2.

c. It helps us to represent forces and displacements at the element level.

corresponding to every node in the overall structure, there will be as many sets of local co-ordinates as there are elements joining at the node under consideration.

d. The matrix which transforms any desired information of the structure to its corresponding element information or vice-versa is termed as transformation matrix.

$$e. f = \frac{l}{AE}$$

f. The element stiffness matrix is the inverse of element flexibility matrix and vice-versa.

$$\text{i.e. } k_e = \frac{1}{f} \quad \text{or} \quad R_e = \frac{1}{f}$$

1-338

g. The stiffness co-efficient R_{ij} is defined as the force developed at joint 'i' due to a unit displacement at joint 'j', while other joints are assumed to be fixed.

h. Displacements are considered as the unknown quantities ~~parameters to be solved~~.

i. All the steps in the stiffness method can be executed by a computer more conveniently. As the solution procedure is unique. It depends on the user for the choice of the primary structure. Hence, programming is simplified. The structure stiffness matrix for a stable linear structure is invariably a well-conditioned matrix, thereby facilitating accurate solutions of the response.

j. $i = (6m + r) - b_j$

External indeterminacy = 18

Internal indeterminacy = 6

PART-B

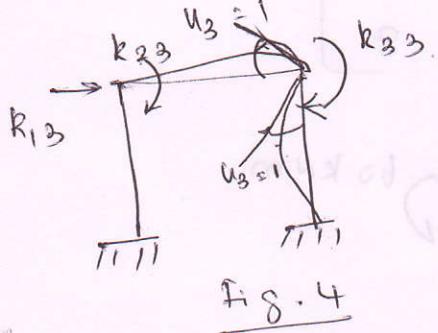
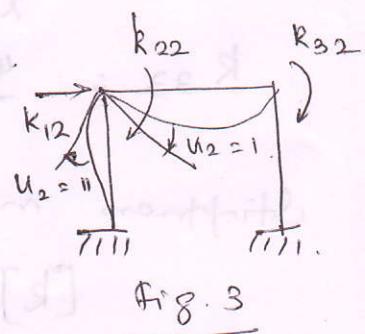
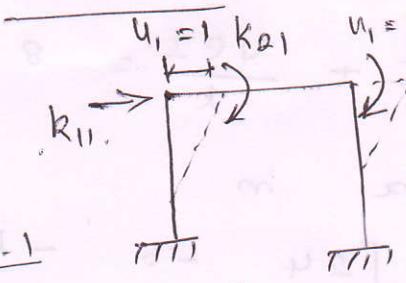
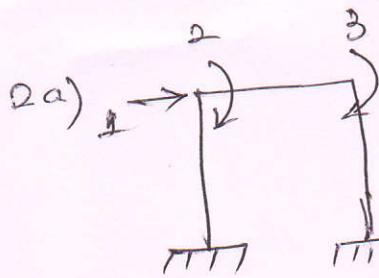


Fig. 1

stiffener
co-ord.

matrix to be developed for
nodes 1, 2 and 3:

To generate 1st column of the stiffener matrix,
apply unit displacement @ coordinate 1
as shown in fig. 2.

$$R_{11} = \frac{12EI}{l^3} + \frac{12EI}{l^3} = 24.$$

$$R_{21} = -\frac{6EI}{l^2} = -6;$$

$$R_{31} = -\frac{6EI}{l^2} = -6.$$

To generate 2nd column, apply unit displacement
at 2..

$$R_{12} = -\frac{6EI}{l^2} = -6; \quad R_{22} = -\frac{4EI}{l^2} + \frac{4EI}{l} = 8$$

$$R_{32} = \frac{2EI}{l} = 2.$$

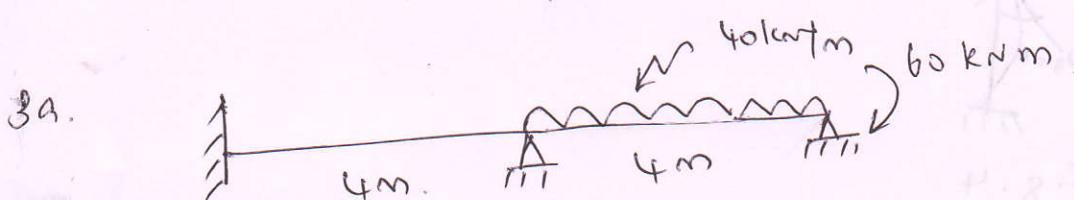
To generate 3rd column, apply unit
displacement at 3

$$R_{13} = \frac{-6EI}{l^2} = -6; \quad R_{23} = \frac{2EI}{l} = 2;$$

$$R_{33} = \frac{4EI}{l} + \frac{4EI}{l} = 8.$$

Stiffness matrix is

$$[k] = \begin{bmatrix} 24 & -6 & -6 \\ -6 & 8 & 2 \\ -6 & 2 & 8 \end{bmatrix}$$



Ques.

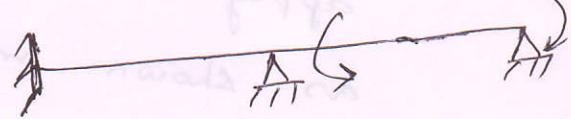
(1) Fixed end moments.

$$M_{FA} = M_{FBA} = 0$$

$$M_{FBC} = M_{FCB} = -\frac{40 \times 4^2}{12} = -53.33 \text{ kNm.}$$

$$= +53.33 \text{ kNm}$$

$$\{P^0\} = \begin{cases} 0 \\ 0 \\ -53.33 \\ +53.33 \end{cases} \text{ kNm.}$$



Fixed end moments

(2) Static indeterminacy = 2

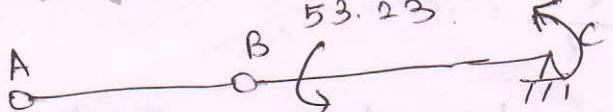
Introduce hinges at A and B.

Introduce hinges at A and B.



Determinate

structure.



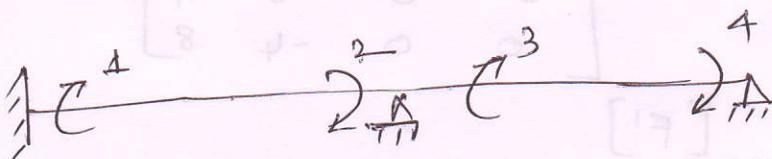
Unbalanced moment.

13.35

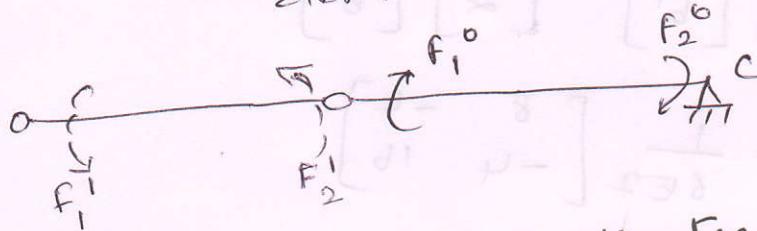
6. 67



Balanced Moment.



Element co. ordinates.



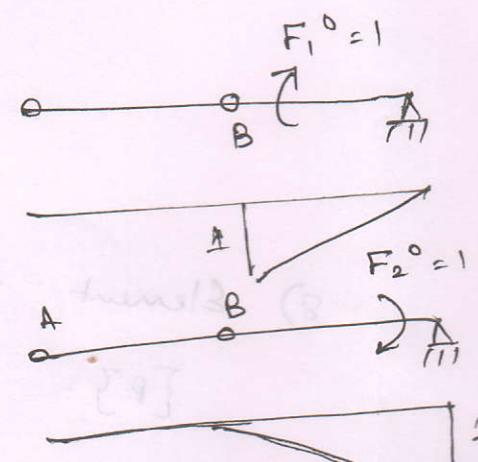
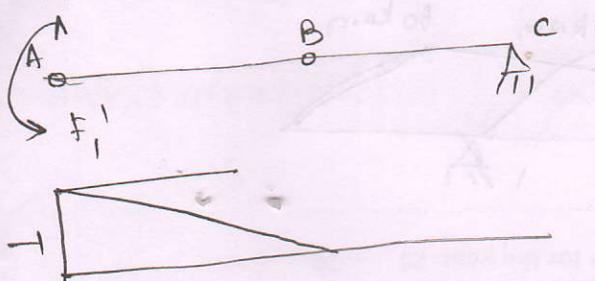
System coordinates

$$[F^0] = \begin{bmatrix} 53.33 \\ 6.67 \end{bmatrix}$$

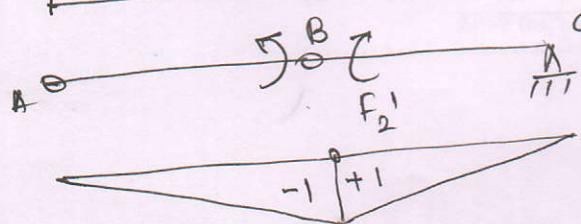
3) Apply unit forces (moment) $F_1^0 + F_2^0 @ 3^{rd}$

4th co. ordinates separately

$$[b^0] = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 1 & 0 \\ 0 & 1 \end{bmatrix}$$

4) Apply unit redundant forces
 $F_1^1 + F_2^1$ to generate 1st + 2nd
columns of $[b^1]$ 

$$[b^1] = \begin{bmatrix} -1 & 0 \\ 0 & -1 \\ 0 & 1 \\ 0 & 0 \end{bmatrix}$$



5) Element flexibility matrix. $[\alpha]$

$$[\alpha] = \frac{1}{6EI} \begin{bmatrix} 8 & -4 & 0 & 0 \\ -4 & 8 & 0 & 0 \\ 0 & 0 & 8 & 4 \\ 0 & 0 & -4 & 8 \end{bmatrix}$$

6) To generate $[F^e]$

$$[a_{11}] = [b^e]^T [\alpha] [b^e]$$

$$= \frac{1}{6EI} \begin{bmatrix} 8 & -4 \\ -4 & 16 \end{bmatrix}$$

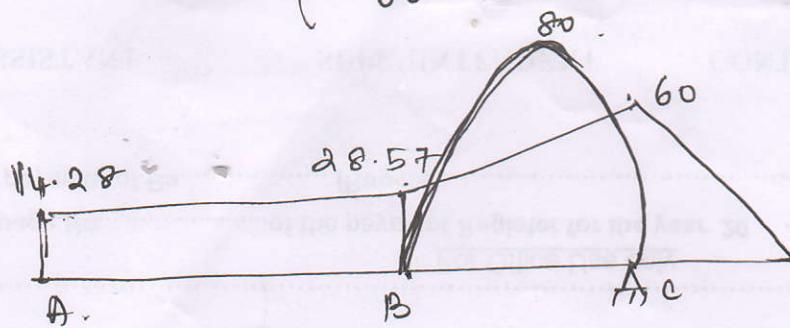
$$\Rightarrow \{F^e\} = -[a_{11}]^{-1} [a_{10}] \{F^0\}.$$

$$\begin{aligned} &= -[a_{11}]^{-1} [b^e]^T [\alpha] [b^0] \{F^0\} \\ &= \begin{Bmatrix} -14.28 \\ -28.57 \end{Bmatrix} \end{aligned}$$

7) Element forces $\{P^e\}$

$$\{P^e\} = [b^0] \{F^0\} + [b^e] \{F^e\} + \{P^0\}.$$

$$= \begin{Bmatrix} 14.28 \\ 28.57 \\ -28.57 \end{Bmatrix} \text{ kNm.}$$



BMD.

4a) Static indeterminacy = 1 owing to

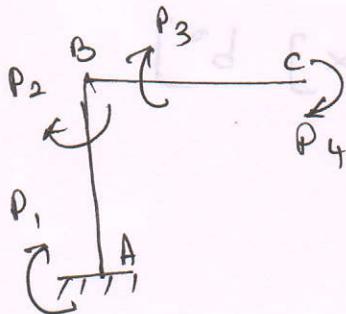
B

C

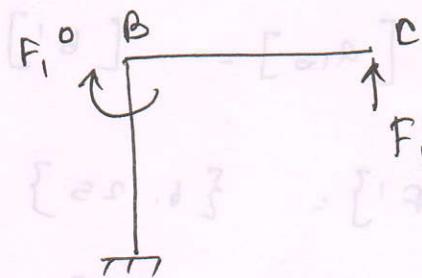
A

Primary structure

Consider ~~the~~ reaction at C as redundant force.

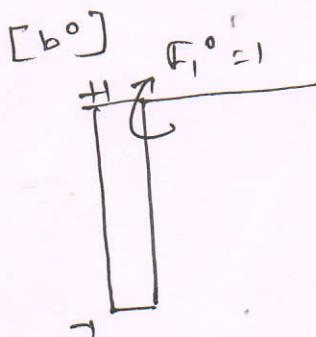


Element Co-ord



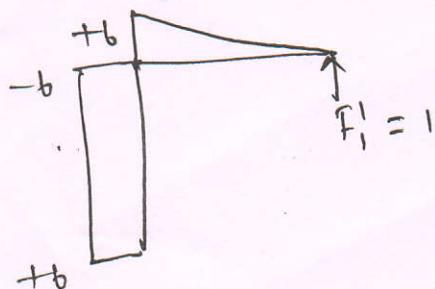
System Co-ord

Apply unit external force F_1^o at B to generate



$$[b^o] = \begin{bmatrix} -1 \\ 1 \\ 0 \\ 0 \end{bmatrix}$$

Apply unit redundant force F_1' to generate [b]



$$[b] = \begin{bmatrix} b \\ -b \\ b \\ 0 \end{bmatrix}$$

Element flexibility matrix $[\alpha]$

$$[\alpha]_E = \frac{6}{6EI}$$

$$\begin{bmatrix} 2 & -1 & 0 & 0 \\ 0 & 9 & 0 & 0 \\ 0 & 0 & 2 & -1 \\ 0 & 0 & -1 & 2 \end{bmatrix}$$

To generate $\{F'\}$

$$\{F'\} = -[a_{11}]^{-1} [a_{10}] \{F^0\}$$

standard form

Where

$$[a_{11}] = [b']^T [\alpha] [b']$$

$$[a_{10}] = [b']^T [\alpha] b^0$$

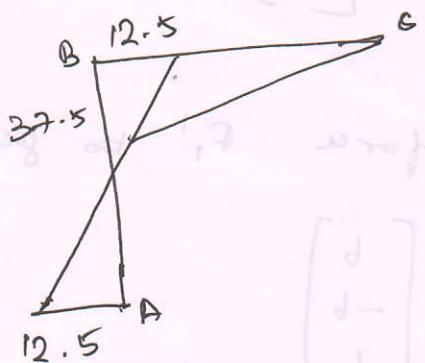
$$\{F'\} = \{b. 25\}$$

Element forces $\{P\}$

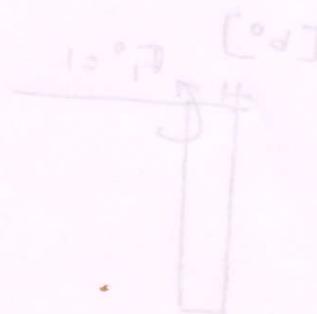
$$\text{Forces at } \{P\} = [b^0] \{F^0\} + [b'] \{F'\}$$

$$\text{Forces at } \{P\} = [b^0] \{F^0\} + [b'] \{F'\}$$

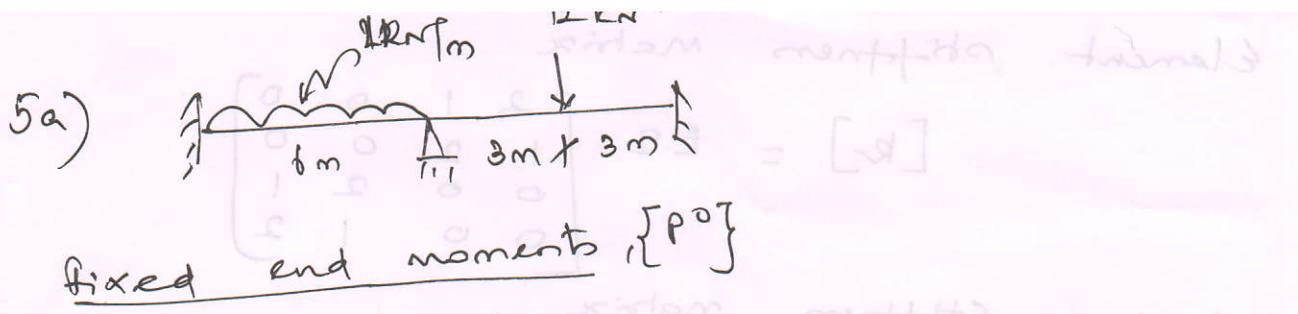
$$= \begin{Bmatrix} -12.5 \\ 12.5 \\ 37.5 \\ 0 \end{Bmatrix} \text{ kNm.}$$



$$\begin{bmatrix} d \\ d \\ d \\ 0 \end{bmatrix} = \begin{bmatrix} d \\ d \\ d \\ 0 \end{bmatrix}$$



$$\begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 1 & 0 & 0 & 0 \\ -1 & 1 & 0 & 0 \end{bmatrix} \frac{d}{133} = \begin{bmatrix} d \\ d \\ d \\ 0 \end{bmatrix}$$



$$M_{FAB} = \frac{-2 \times b^2}{12} = -b \text{ kNm}$$

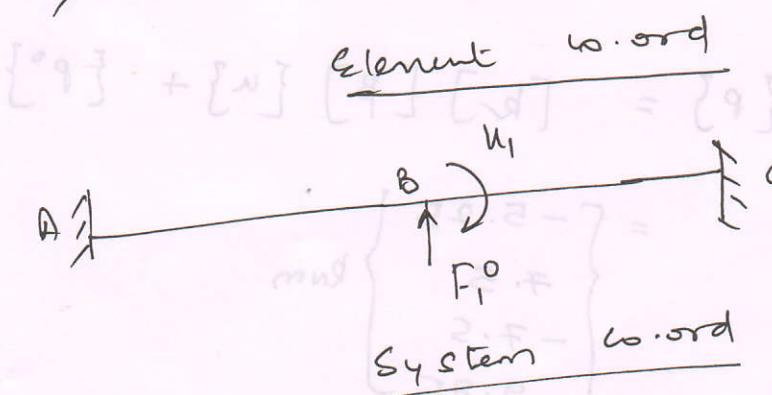
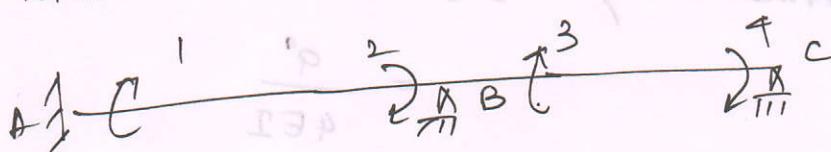
$$M_{FCB} = +6 \text{ kNm}$$

$$M_{FBC} = \frac{-12 \times b}{8} = -9 \text{ kNm}$$

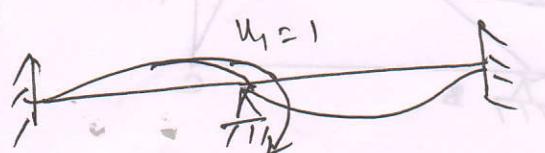
$$M_{FCB} = +9 \text{ kNm}$$

$$\{P^o\} = \begin{Bmatrix} -6 \\ 6 \\ -9 \\ 9 \end{Bmatrix}$$

Kinematic indeterminacy = 1



Apply unit displacement to generate $[P]$



$$[P] = \begin{Bmatrix} 0 \\ 1 \\ 1 \\ 0 \end{Bmatrix}$$

Element stiffness matrix

$$[k] = EI \begin{bmatrix} 2 & 1 & 0 & 0 \\ 1 & 2 & 0 & 0 \\ 0 & 0 & 2 & -1 \\ 0 & 0 & -1 & 2 \end{bmatrix}$$

System stiffness matrix

$$[K] = [\beta]^T [k] [\beta]$$

$$= \frac{4EI}{3}$$

$$[K]^{-1} = \frac{3}{4EI}$$

$$\text{To generate } \{\bar{F}\} = \{F\}^f - [\beta]^T \{P^o\}$$

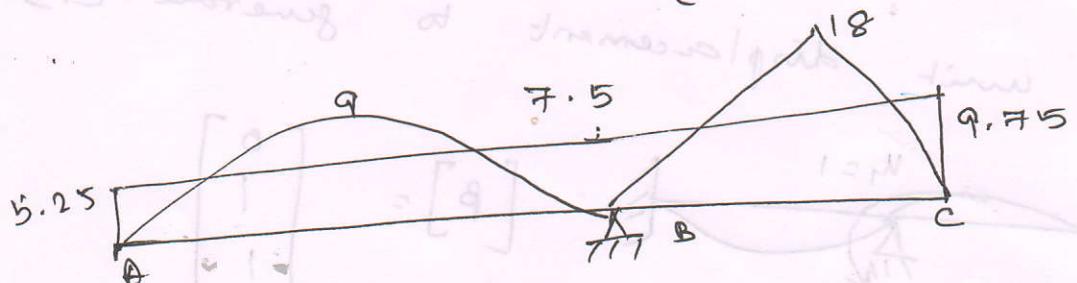
$$= \{3\}$$

$$\text{System deformation, } \{u\} = [K]^{-1} \{\bar{F}\}$$

$$= \frac{9}{4EI}$$

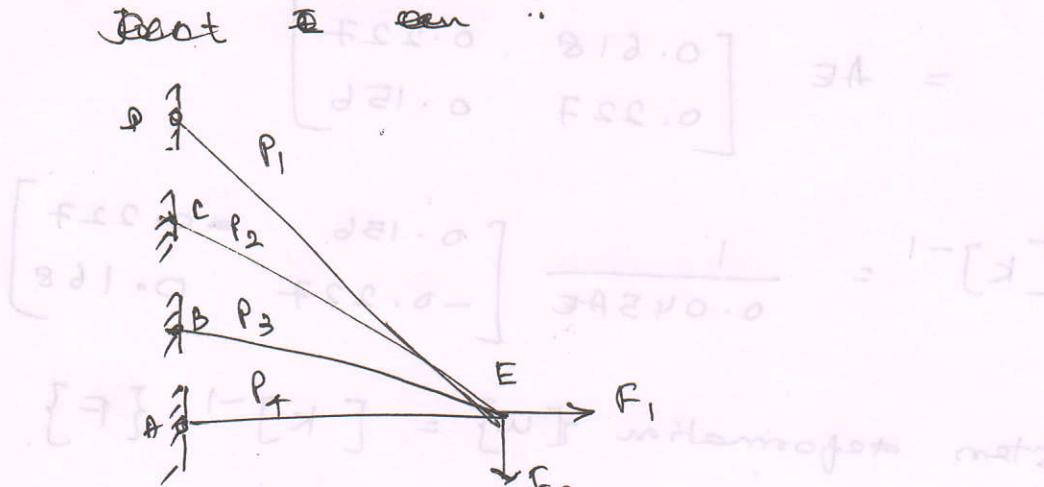
$$\text{Element force, } \{P\} = [k] [\beta] \{u\} + \{P^o\}$$

$$= \begin{Bmatrix} -5.25 \\ 7.5 \\ -7.5 \\ 9.75 \end{Bmatrix} \text{ kNm}$$



BND

6a) degrees of freedom = 2.



System co-ord & Element co-ord.

$$\text{External load vector, } \{F\} = \begin{Bmatrix} 200 \\ 100 \end{Bmatrix}$$

To generate force transformation matrix [E]

Consider equilibrium of joint E

$$F_1 = P_1 \cos 45^\circ + P_2 \cos 33.69^\circ + P_3 \cos 18.43^\circ$$

$$F_2 = P_1 \sin 45^\circ + P_2 \sin 33.69^\circ + P_3 \sin 18.43^\circ$$

$$[E] = [\beta]^T \begin{bmatrix} 0.707 & 0.707 \\ 0.832 & 0.555 \\ 0.949 & 0.316 \\ 0 & 0 \end{bmatrix}$$

To generate element stiffness matrix [k]

$$[k_e] = AE \begin{bmatrix} 1/6.364 & 0 & 0 & 0 \\ 0 & 1/5.408 & 0 & 0 \\ 0 & 0 & 1/4.743 & 0 \\ 0 & 0 & 0 & 1/4.5 \end{bmatrix}$$

System stiffness matrix $[K] = [\beta]^T [k_r] [\beta]$

$$= AE \begin{bmatrix} 0.618 & 0.227 \\ 0.227 & 0.156 \end{bmatrix}$$

$$[K]^{-1} = \frac{1}{0.045AE} \begin{bmatrix} 0.156 & -0.227 \\ -0.227 & 0.168 \end{bmatrix}$$

System deformation $\{u\} = [K]^{-1} \{F\}$.

$$\begin{bmatrix} 0.027 \\ 0.01 \end{bmatrix} = \frac{1}{AE} \begin{bmatrix} 188.89 \\ -635.55 \end{bmatrix}$$

Element forces $\{P\} = [k_r] [\beta] \cdot \{u\}$

$$\{P\} = \begin{Bmatrix} -49.69 \\ -36.22 \\ -4.23 \\ 41.93 \end{Bmatrix} \text{ kN}$$

a) fixed end moments $\{P^0\}$

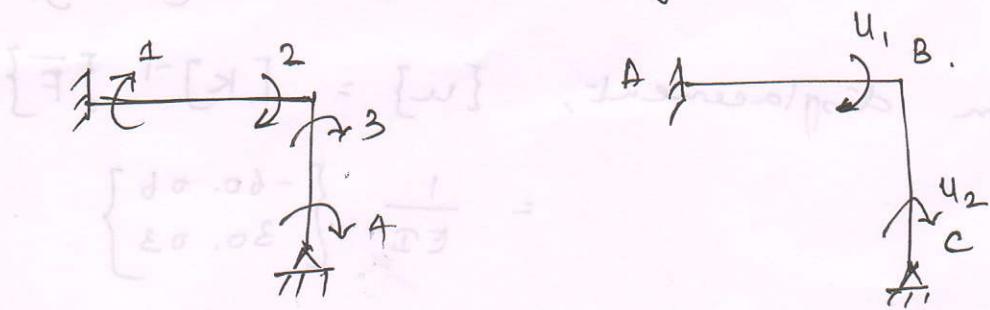
$$M_{FAB} = \frac{-wl^2}{12} = -180 \text{ kNm}$$

$$M_{FBA} = +180 \text{ kNm}$$

$$M_{FBc} = M_{FcB} = 0$$

$$\{P^0\} = \begin{Bmatrix} -180 \\ +180 \\ 0 \\ 0 \end{Bmatrix}$$

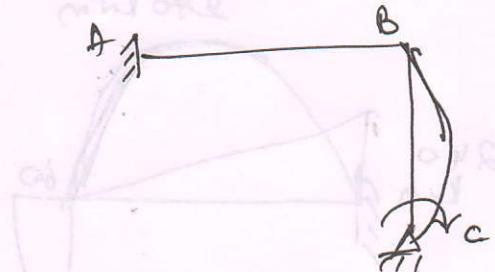
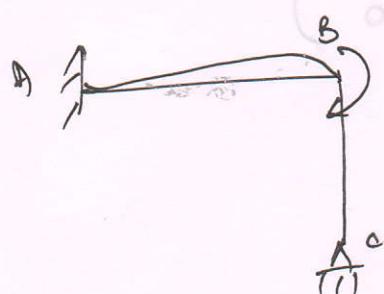
Kinematic indeterminacy = 2



{⁰⁹} Element w. ord

{⁰⁹} System w. ord

Apply unit displ. @ 3rd & 4th w. ord.
to generate 1st + 2nd columns of $[\beta]$.



$$[\beta] = \begin{bmatrix} 0 & 0 \\ 1 & 0 \\ 0 & 0 \\ 0 & 1 \end{bmatrix}$$

kinematics frame

Element stiffness matrix, $[k] = EI \begin{bmatrix} 2 & 1 & 0 & 0 \\ 1 & 2 & 0 & 0 \\ 0 & 0 & 4/3 & 2/3 \\ 0 & 0 & 2/3 & 4/3 \end{bmatrix}$

System stiffness matrix, $[k] = [\beta]^T [k] [\beta]$

$$[k] = EI \begin{bmatrix} 10/3 & 2/3 \\ 2/3 & 4/3 \end{bmatrix}$$

$$[k]^{-1} = \frac{1}{4EI} \begin{bmatrix} 4/3 & -2/3 \\ -2/3 & 10/3 \end{bmatrix}$$

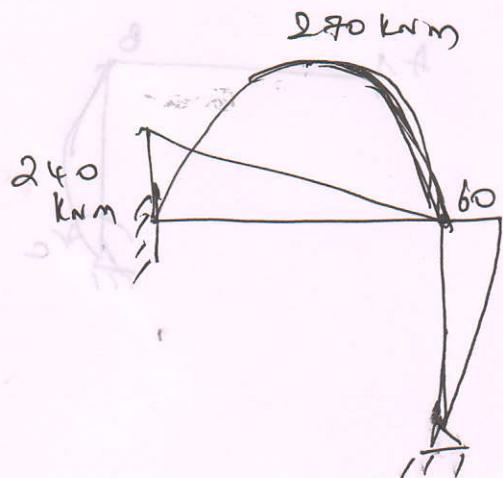
$$\{\bar{F}\} = \{F\}^f - [B]^T \{P^o\} = \begin{Bmatrix} -180 \\ 0 \end{Bmatrix} \text{ kN}$$

system displacement, $\{u\} = [K]^{-1} \{\bar{F}\}$

$$= \frac{1}{EI} \begin{Bmatrix} -60.06 \\ 30.03 \end{Bmatrix}$$

Element forces, $\{P\} = [k_e] [B] \{u\} + \{P^o\}$

$$= \begin{Bmatrix} -240 \\ 60 \\ -60 \\ 0 \end{Bmatrix}$$



B me

8.9) Techniques used to reduce memory requirement for storing the stiffness matrix

(1) Use of symmetry & banded nature

(2) Partitioning of matrix

(3) Skyline storage.

Explanation on the above types.

$$\begin{bmatrix} \text{elt} & \text{elt} \\ \text{elt} & \text{elt} \end{bmatrix} \xrightarrow{\text{Exp}} = \begin{bmatrix} \text{elt} \\ \text{elt} \end{bmatrix}$$